

Claims

1 A method for modeling an object composed of one or more components,
2 comprising:
3 inputting data for each component of the object, the data including
4 Cartesian coordinates expressed in Euclidean space of a plurality of points \mathbf{x}
5 of each component;
6 encoding each point \mathbf{x} as a vector x in a general homogeneous space
7 by $x = (\mathbf{x} + \frac{1}{2}\mathbf{x}^2 e + e_*)E = \mathbf{x}E - \frac{1}{2}\mathbf{x}^2 e + e_*$, where e and e_* are basis null
8 vectors of a Minkowski space E ; and
9 associating a plurality of general homogeneous operators with each
10 data construct to generate a model of the object.

1 2. The method of claim 1 further comprising:
2 supplying run-time parameters for the plurality of operators; and
3 applying the plurality of general homogeneous operators to each
4 encoded point \mathbf{x} of each associated component to manipulate the model of
5 the object.

1 3. The method of claim 1 further comprising:
2 measuring a scalar \mathbf{d}_{ab} between two component points \mathbf{a} and \mathbf{b}
3 encoded as general homogeneous points a and b by $\mathbf{d}_{ab}^2 = (a - b)^2 = -2a \bullet b$.

1 4. The method of claim 1 wherein a line through component points **a** and **b**
2 encoded as general homogeneous points a and b is modeled by $e \wedge a \wedge b$, and a
3 length l_{ab} of a line segment connecting component points **a** and **b** is
4 $(l_{ab})^2 = (e \wedge a \wedge b)^2 = (a - b)^2$.

1 5. The method of claim 1 wherein a plane through component points **a**, **b**,
2 and **c** encoded as general homogeneous points a , b , and c is modeled by
3 $e \wedge a \wedge b \wedge c$, and an area A_{abc} defined by component points **a**, **b**, and **c** is
4 $(A_{abc})^2 = \frac{1}{4} (e \wedge a \wedge b \wedge c)^2$.

1 6. The method of claim 1 wherein a sphere s with radius r centered at a
2 component point **c** encoded as a general homogenous radius r and center c
3 is generated by a vector $s = c + \frac{1}{2} r^2 e$.

1 7. The method of claim 1 wherein a sphere s determined by four component
2 points **a**, **b**, **c**, **d** encoded as general homogeneous points a, b, c, d is generated
3 by $s = IE (a \wedge b \wedge c \wedge d)$, where I is a largest k -blade.

1 8. The method of claim 7 wherein one of the general homogeneous points
2 a, b, c, d is equal to the point e so that s defines a plane through the point e .

1 9. The method of claim 5 wherein a distances between a component point **a**
2 and a component plane **p** is an inner products $a \cdot p$ of an encoded point a and
3 an encoded plane p .

1 10. The method of claim 6 wherein a distances between a component point **a**
2 and a component sphere **s** is an inner product $a \bullet s$ of and encoded point a and
3 the encoded sphere p .

1 11. The method of claim 6 wherein a distance between two component
2 spheres s_1 and s_2 encoded as spheres $s_1 = c_1 + \frac{1}{2}r_1^2 e$ and $s_2 = c_2 + \frac{1}{2}r_2^2 e$ is
3 generated by $s_1 \bullet s_2 = c_1 \bullet c_2 + \frac{1}{2}(r_1^2 + r_2^2) = -\frac{1}{2}[(c_1 - c_2)^2 - (r_1^2 + r_2^2)]$.

1 12. The method of claim 1 wherein the object is a rigid body, and a motion
2 of the rigid body is determined by a time dependent displacement versor
3 $D=D(t)$ satisfying a differential equation $\dot{D} = \frac{1}{2}VD$, with "screw velocity" V
4 given by $V = -I\omega + e\mathbf{v}$, where ω is a velocity and \mathbf{v} is a translational velocity
5 of the rigid body.

1 13. The method of claim 12 wherein *dynamics* of the rigid body are
2 determined by a differential equation $\dot{P} = W$, where $P = -I\mathbf{L} + e_*\mathbf{p}$, and
3 $W = -I\mathbf{T} + e_*\mathbf{F}$, where \mathbf{L} is an angular momentum and \mathbf{p} is a translational
4 momentum of the rigid body, while \mathbf{T} is the a torque and \mathbf{F} is a net force on
5 the rigid body.

1 14. The methods of claim 12 wherein the rigid body includes n linked rigid
2 components, and a motion of the rigid body is modeled by n time dependent
3 displacement versors D_1, D_2, \dots, D_n , and a motion of a k^{th} linked rigid
4 component is determined by a versor product $D_1 D_2 \dots D_k$.

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